Using Variable-Fidelity Models in Multidisciplinary Design Optimization

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The Engineering Multidisciplinary Optimization (MDO) Problem...

...can be stated as

minimize
$$f(x,u(x))$$
 subject to $h(x,u(x))=0$ $g(x,u(x))\geq 0,$

where, given design variables x, the state variables u(x) are defined via

$$A(x,u(x)) = \left(egin{array}{c} A_1(x,u_1(x),\ldots,u_N(x)) \ dots \ A_N(x,u_1(x),\ldots,u_N(x)) \end{array}
ight) = 0,$$

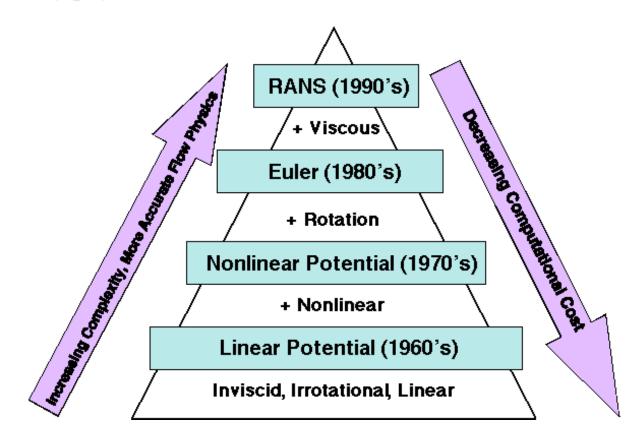
The blocks of the system usually represent the state equations for the disciplinary analyses and the necessary interdisciplinary couplings.

Motivation

- Address computational expense of repeated use of high-fidelity models
 - Solutions of coupled PDE typically required at each iteration
 - For uncoupled problem formulations, the number of function evaluations typically rises
 - The difficulty is not likely to disappear with improvements in computational technology
 - Use of lower-fidelity models alone does not guarantee improvement in higher-fidelity design
 - Variable-fidelity models in use for a long time
- Allow for easier integration of disciplines in MDO
- Allow for interactive design
- Demonstrate feasibility of proposed methods on engineering problems

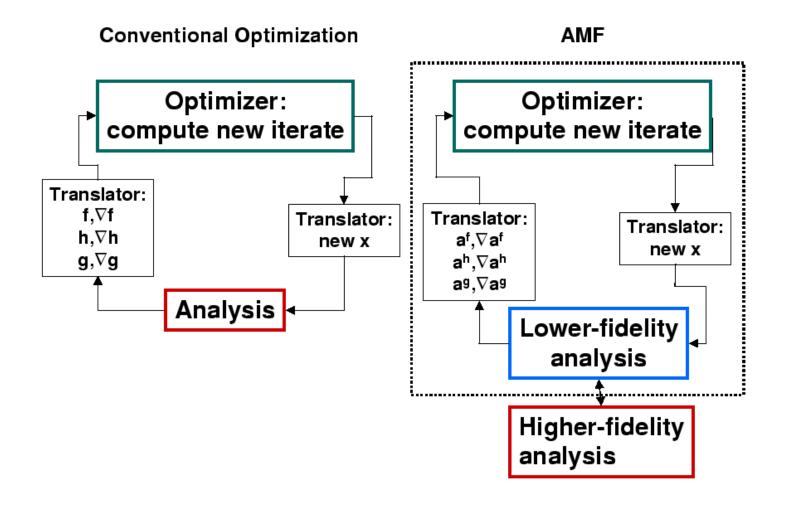
Example: Variable-Fidelity Computational Models in CFD

• Variable-fidelity physical models (Jameson, 1997)



- A single physical model evaluated on meshes of varying refinement
- Polynomial approximations such as RSM, kriging

Conventional Optimization vs. Approximation Management



Some Related Work

- Overview of approximation concepts in structural design, Barthelemy and Haftka 1993
- Research conducted or supported at NASA Langley:
 - Design-oriented analysis, Gumbert et al., Silva et al. (NASA LaRC), Haftka at al. (University of Florida/VPI)
 - A posteriori error bounds for outputs of PDE and sensitivity derivatives of outputs, Lewis (ICASE), Patera et al. (MIT)
 - Managing models/approximations in optimization, Alexandrov et al. (NASA LaRC)
- Managing approximations in optimization, Booker et al. (Boeing/IBM/Rice/W&M)

A First-Order AMF for Constrained Optimization

- Potentially as many AMF's as there are optimization algorithms
- The underlying algorithm MAESTRO (Alexandrov '93, Alexandrov and Dennis '98)
- Control "the amount" of optimization by varying the size of the trust region
- Not necessary to change physical models to obtain convergence
- When other models available, guidance on alternating
- Easily applicable to MDO problems

AMF: model of constraints and substep

- Consider minimize $\{f(x):h(x)=0\}$, where f and h are expensive
- ullet Let x_c be the current iterate and Δ_c be the trust-region radius; set $z_0=x_c$
- At x_c , select a model of the constraints a_c^h that satisfies:

$$a_c^h(x_c) = h(x_c)$$

$$\nabla a_c^h(x_c) = \nabla h(x_c)$$

• Find a substep s_1 that approximately solves:

minimize
$$a_c^h(z_0+s)$$

subject to $\parallel s \parallel \leq \theta \Delta_c, \ \theta \in (0.5,0.6)$

• Set $z_1 = z_0 + s_1$

AMF: model of objective and substep

• Select a model a_c^f of the objective function that satisfies:

$$a_c^f(x_c + s_1) = f(x_c + s_1)$$

$$\nabla a_c^f(x_c + s_1) = \nabla f(x_c + s_1)$$

• Find s_2 that approximately solves:

minimize
$$a_c^f(z_1+s)$$
 subject to $\parallel s \parallel \leq \sqrt{\Delta_c^2 - \lVert s_1 \rVert^2}$

- Set $s_c = s_1 + s_2$
- An extension of MAESTRO—the Gauss-Newton model of the constraints and the quadratic model of the objective replaced by general models that satisfy first-order consistency conditions

AMF: evaluating the step / updating

- Merit function: $\mathcal{P}(x; \rho) \equiv f(x) + \rho \parallel h(x) \parallel^2$ or $\mathcal{L}(x, \lambda; \rho) \equiv f(x) + \lambda^T h(x) + \rho \parallel h(x) \parallel^2$
- Penalty parameter ρ (not used in computing the step) is updated in rigorously (El-Alem, 1987)
- Define

$$ar d_c \equiv \mathcal{P}(x_c; \rho_c) - \mathcal{P}(x_c + s_c; \rho_c)$$

and

$$pr \ d_c \equiv \left[f(x_c) - a_c^f(x_c + s_c) \right] +
ho_c \left[\parallel h(x_c) \parallel^2 - \parallel a_c^h(x_c + s_c) \parallel^2
ight]$$

ullet Update the iterate and Δ_c based on $r=rac{ared_c}{pred_c}$

AMF: conditions on the trial step

- To inherit convergence properties from MAESTRO, s_1 and s_2 must satisfy:
 - A sufficient decrease condition: s_c is to satisfy a fraction of Cauchy decrease in model k
 - A boundedness condition: s_1 to satisfy

$$\parallel s_1 \parallel \leq \mathcal{K} \parallel h(x_c) \parallel$$

for some constant K independent of the iterates

• Both are easily satisfied; another trust-region procedure suffices

One choice of trial step—constraints (objective analogous)

Convergence properties

• Theoretical:

- MAESTRO assumptions: smoothness and boundedness, full rank for the gradients of constraints and their models, sufficient decrease and boundedness for the substeps
- AMF assumptions: consistency conditions and uniform boundedness of the Hessian approximations
- Result: first-order convergence to a critical point of the high-fidelity problem

• Practical:

- Enforce compatibility conditions
- Actual performance will depend on the predictive properties of the model; very problem-dependent

Preliminary Numerical Results

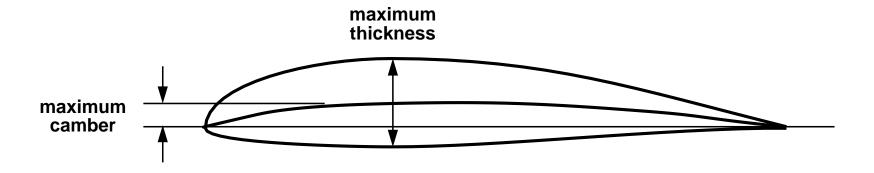
- Initial testing on Hock and Schittkowski problems and MDOB Test Suite problems; notion of variable-fidelity models not well defined
- Now demonstrating feasibility on single-discipline, aerodynamic optimization problems
- Variable-fidelity models represented by a single model evaluated of meshes of varying refinement
- Computational experiment:
 - Single-fidelity problems solved with a well-known optimizers
 - Single-fidelity problems solved with a research implementation of MAESTRO, without AMF
 - Variable-fidelity problem solved with MAESTRO-based AMF

Preliminary Numerical Results: computational details

- Consistency conditions:
 - Enforced only at "major" iterates
 - Can be relaxed
 - Are easily enforced (Chang et al. '93):
 - * Given $f_{hi}(x)$ and $f_{lo}(x)$, define $\beta(x) \equiv \frac{f_{hi}(x)}{f_{lo}(x)}$
 - * Given x_c , build $\beta_c(x) = \beta(x_c) + \nabla \beta(x_c)^T (x x_c)$
 - * Then $a_c(x) = \beta_c(x) f_{lo}(x)$ satisfies the consistency conditions
- Inequality constraints handled by squared slacks

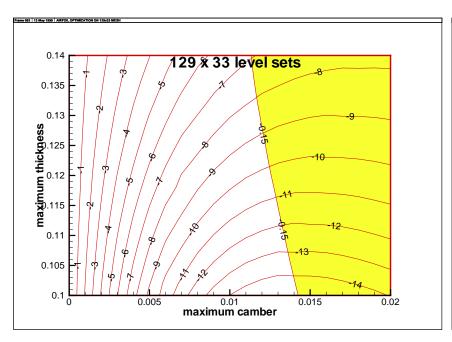
Preliminary Numerical Results: 2D Airfoil Optimization Problem formulated and assembled by L.L. Green

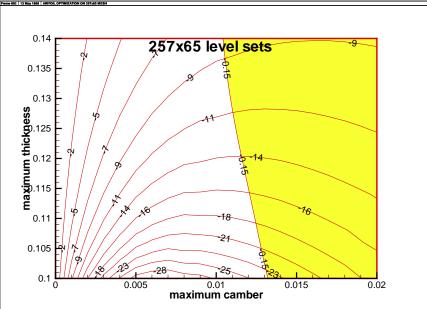
• Objective: $-\frac{L}{D}$



- Constraints: pitching moment
- Design variables: maximum camber, maximum thickness
- Analysis: Euler (NS/Euler code FLOMG, Swanson, Turkel)
- Conditions: subsonic, inviscid flow
- Levels of fidelity: analyses on 129x33, 257x65 meshes

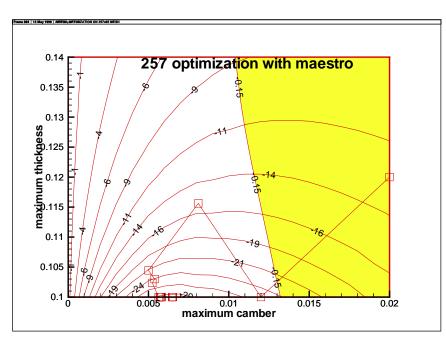
2D Airfoil: Problem Description

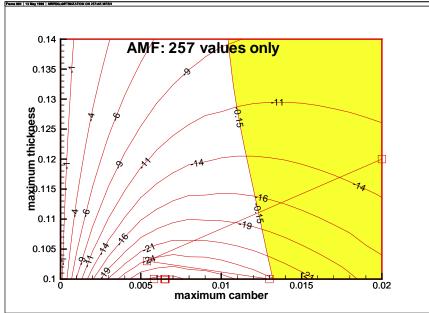




- Time/analysis on 257x65 mesh = 4 Time/analysis on 129x33 mesh
- Approximately 8 min vs 2 min per analysis cold start (free stream conditions)
- Restart files are used neighboring solutions obtained more efficiently

2D Airfoil: MAESTRO and AMF Results



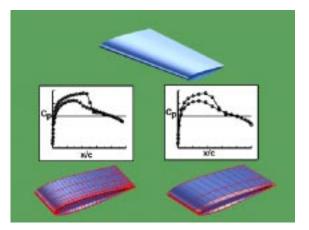


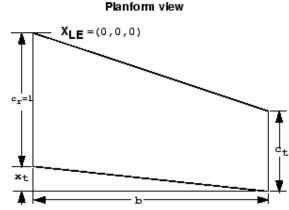
• Number of iterations:

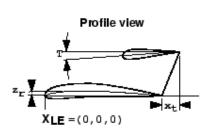
- MAESTRO: 257 mesh alone 34
- AMF: on 129 mesh 20; on 257 mesh 9; equivalent 257 mesh 14

Preliminary Numerical Results: 3D Wing Optimization Problem formulated and assembled by C.R. Gumbert

• Objective: $-\frac{L}{D}$

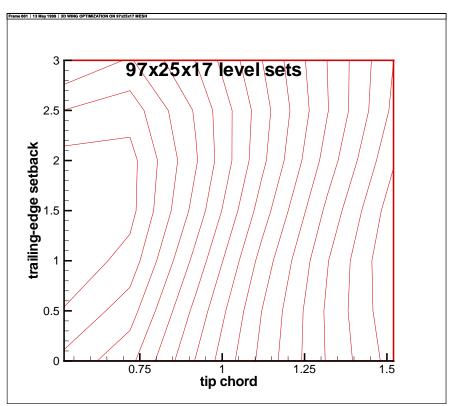


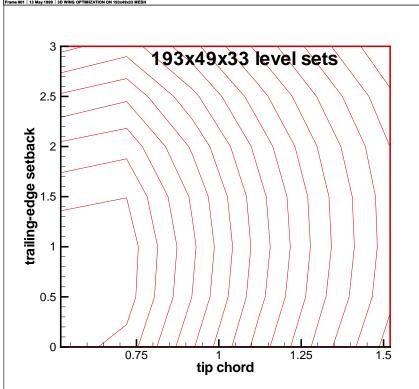




- Constraints: $C_L S$ (total lift); C_l (rolling moment); C_M (pitching moment)
- Design variables: tip chord, trailing edge setback
- Analysis: Euler (NS/Euler code CFL3D, NASA LaRC)
- Conditions: subsonic, inviscid flow
- Levels of fidelity: analyses on 97x25x17, 193x49x33 meshes

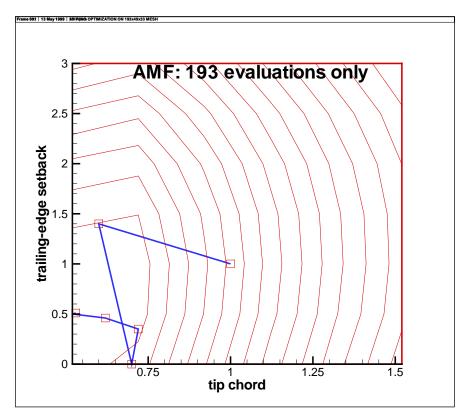
3D Wing: Problem Description





- Time/analysis on 193x49x33 mesh = 8 Time/analysis on 97x25x17 mesh
- Approximately 64 min vs 8 min per analysis, cold start (free stream conditions)
- Restart files are used

3D Wing: MAESTRO and AMF Results



- Constraints were inactive for this regime
- Number of iterations:
 - MAESTRO: 97 mesh alone 17; 193 mesh alone in progress, expect similar
 - AMF: 97 mesh 17; 193 mesh 7; equivalent 193 mesh 9

Conclusions to-Date

- Initial numerical results with MAESTRO-based AMF are promising
- For models represented by variable mesh sizes, must use consistent families of meshes
- Demonstration with engineering analysis codes is difficult
 - Standard practice: re-grid at new points; do not take long steps
 - We are attempting to use mesh deformation and may take long steps
 - Robustness wrt mesh deformation in question
 - Results sensitive to analysis convergence
 - Analysis and derivatives very sensitive to feasible region (bounds)
- Test problem characteristics typical for some classes of problems only
- For other problems other models have to be considered

Currently Under Investigation

- Strategies for maximizing the use of lower-fidelity models (e.g., using information from *a posteriori* bounds for PDE outputs)
- Other CFD problem regimes (e.g., transonic)
- A variety of approximations and AMF's
- Other model arrangements (variable-fidelity physical, reduced-order models)
- Using automatic differentiation for generating derivatives
- Demonstrations for multidisciplinary problems